

ORIGINAL ARTICLE

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The energy potential of soft rush (*Juncus effusus* L.) in different conversion routes

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Abstract

Background: Rushes are prominent wetland plants that are well adapted to conditions of waterlogging. Tall rushes like soft rush (*Juncus effusus* L.) tend to dominate the vegetation and offer a great biomass potential. Removing rush biomass is often necessary to enhance various ecosystem services of wetlands. There is an urgent need for sustainable use of the removed biomass apart from expensive composting or useless landfill.

Methods: We investigated three alternative energy utilisation routes for soft rush biomass and evaluated their energetic potential: biomethanisation via wet fermentation technique (a), biomethanisation via solid-state fermentation technique (b) and combustion (c). Batch experiments (a), experimental fermenters (b), and thermo-calorimetric equipment (c) were used to measure energy output per unit rush biomass input.

Results: The wet fermentation technique had significantly higher biogas yields than solid-state fermentation (399 L_N kg⁻¹ oDM compared to 258 L_N kg⁻¹ oDM). These yields constitute 59 and 43%, respectively, of the biogas potential of maize silage as a reference. Solid-state fermentation technique needs longer retention time compared to wet co-digestion to earn comparable methane yields. Soft rush biomass shows high heating values (15.06 MJ kg FM_{w15}⁻¹) compared to other herbaceous solid fuels.

Conclusions: Low costs for substrate production make energetic utilisation of *Juncus effusus* an interesting alternative, if short distances between fields and biomass conversion plant can be realised. All investigated conversion routes appear promising, provided that the substrate specifics are considered in the design of the conversion technique. Besides the size of the rush dominated area and the distribution of these areas in the landscape, the investment costs and the subsidies for the conversion plant play a pivotal role in the selection of the preferred conversion path.

Keywords: Wetland biomass, Soft rush, Energetic conversion, Biogas, Direct thermal utilisation, Solid-state fermentation, Wet co-digestion

Background

Rushes are prominent wetland plants of the genus *Juncus*, occurring with more than 200 species worldwide in a broad range of habitats [1]. Most of them are helophytes and well adapted to conditions of waterlogging [2]. Soft rush (*Juncus effusus* L.) is a perennial, tussock-forming

and tall growing member of that genus [3, 4]. *Juncus effusus* is widespread throughout subtropical, temperate and boreal regions [3] and often provides crucial eco-system services in natural peat- and wetlands [5–7]. However, if peatlands are meliorated and used for ruminant husbandry, the dominant macrophyte soft rush is regarded as a weed [8] due to its low forage value and high infestation potential [9]. Tall rushes like *Juncus effusus* have the capacity to dominate the vegetation [10], especially under periodically wet conditions and extensive grazing [11]. Both properties, providing ecosystem services in natural

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wetlands and driving out forage grasses in extensively managed peatlands for conservation goals, can be attributed to the impressive viability, the robustness against high iron and sulphide concentrations [12] and the remarkable biomass potential of this species. Tall rush dominated stands can reach aboveground biomass yields more than 10 t dry matter per ha [4, 13].

Despite this ecological performance, rushes have not played a notable role as cultivated crops in paludiculture until now [14]. However, Coleman et al. [15] and Menon and Holland [16] found soft rush suitable as a remediation plant in constructed wetlands. Syranidou et al. [17] highlighted the successful contributions of *Juncus effusus* to clean wastewater in detail. Using rushes as phytoremediation plants can also lead to high yielding stands depending on stress level and nutrient load in the sewage. A removal of biomass enhances proper functionality of sewage clearing in some constructed wetlands [18]. Solutions for further treatment of removed biomass outside organic waste landfills have to be found.

Removing rush biomass is often necessary in semi-natural and extensively used wet grasslands too to enhance the ecosystem services for a variety of reasons like the removal of nutrients [19], reduction of competition [20] or providing habitats for birds [21]. Rush provides almost no value for livestock feeding [22], and if rush stands need to be harvested, it makes sense to utilise the incidental biomass in different ways. A broad scale of technical opportunities for such biomass utilisation in biorefinery exists [23]. Nevertheless, the use for energy purposes seems to be the most promising one [24, 25]. In contrast to the economically superior energy plant maize, rush biomass from wetlands also shows ecological benefits and helps to avoid the food vs. energy conflict [26].

Under the current economic conditions, the procedures of combustion [27] as well as the transformation into biogas [28] are the most viable converting technologies for wetland biomass. These two basic conversion routes place specific, different demands on the biomass properties, which have to be regarded in different technological conversion procedures. While combustion technologies require biomasses with restricted amounts of minerals and N, S, Cl compounds in the dry matter [29] and can use lignocelluloses well [30], biomethanisation is sensitive to high lignified fibre and inhibitive secondary plant compounds in the feed stuff too [31]. Except for the studies of Corton et al. [32], Hensgen et al. [33] and Joseph et al. [34], where biomasses with high amounts of rushes were included, no further conceptual investigation concerning the preferred use of rush biomass according to its contents and material conditions could be found in the relevant scientific databases (ScienceDirect, SCOPUS, Web of Science). This study aimed at filling the gap of knowledge by analysing

the use of rush biomass for energy purposes in different utilisation routes.

The specific questions we addressed against this general background were as follows:

(I) Which conversion route—combustion, wet fermentation or solid-state fermentation is practicable for biomass from *Juncus*-dominated wet grasslands? (II) Which energetic conversion efficacy of the biomass can be attained by the different technologies applied? (III) Which technique should be preferred?

Material and methods

Substrates

Substrates for the conversion techniques were sampled at different peaty grassland areas in Northern Germany where soft rush dominates vegetation coverage. The substrate collections were carried out separately for each of the three conversion routes. In every case, late summer to early autumn sampling dates were chosen to be in line with the common practice of biomass harvest under landscape preservation conditions. Soft rush coverage of the site and standing biomass was roughly estimated using a compressed-height calibrated plate meter (Herbometre®, INRA, France). We harvested the biomasses for both fermentation experiments with motor scythes and for the combustion experiments with a commercial grass shear. An overview of site characteristics, substrate origin, conditioning and further experimental usage is given in Table 1.

Percentage of senescent plant materials in the rush bulks was visually estimated. Rush-dominated stands were cut at a stubble height of 5–7 cm above ground. Thereafter, non-rush plant biomass was separated from the collected harvest stocks. The separated soft rush material was then chopped by hand and mixed afterwards. The biogas feedstocks dedicated for the solid-state fermentation experiments were ensiled in plastic tubs with an ensiling duration of 90 days. In the case of wet fermentation batch trials, the chopped rush substrate was frozen at $-22\text{ }^{\circ}\text{C}$ and defrosted immediately before batch series starts. A representative sample of 500 g fresh matter from the soft rush biomass was dried for further chemical Weender analysis including crude fibre (CF), crude protein (CP) and enzyme-insoluble organic substance (EULOS) determination according to Naumann and Basler [35]. Dry combustion technique (Elementar Analyzer, Vario Max CNS, Elementar®, Germany) has been adapted to determine total carbon (C) and sulphur (S) contents.

Methods

Batch wet co-fermentation test

We used a mini batch test according to the VDI Guideline 4630 [36] as the standard to simulate a

Table 1 Origin and some field characteristics of the rush biomass collected for the different energy conversion experiments

Location	Biomass yield (t ha ⁻¹)	Amount of harvested material (kg FM)	Amount of senescent material (% FM)	Conversion experiment	Substrate conditioning
Darß	2.0–4.0	~ 500	5–30	Solid-state fermentation	Silage from pure rush biomass
Rendsburg	3.5	~ 25	~ 12	Wet fermentation	Fresh rush biomass, thawed after freezing
Rostock	2.8	~ 2.5	~ 7	Combustion	Fresh rush biomass, air-dried

discontinuous wet fermentation under mesophilic temperature conditions. Gas-tight 1-l bottles served as reactors. They were heated up to the desired temperature of 38 °C by placing them in a temperature-controlled water bath (see Fig. 1a). The formed biogas was channelled into gasbags and the volume was determined by drum gas meters (TG, Ritter®, Germany). Because of the small amounts of substrate and consequently of biogas too, the time of the qualitative gas analysis was determined by a minimum threshold of 500 ml produced biogas.

The substrates were inoculated with decomposed fermentation residue from a biogas plant by a mass ratio of < 0.5 referred to the content of organic substance (w/w). After starting the fermentation in three replications, the

formed gas volumes and external conditions were recorded daily. The biogas composition (CH₄, CO₂, O₂) was determined with a biogas monitor (bm 2000, Ansyco®, Germany) if sufficient biogas was available. After a holding time of 35 days, the biogas yield of the soft rush substrate was calculated and corrected to standard volumes taking the environmental conditions, the biogas yield of the inoculum and the methane proportion into account.

Batch solid-state fermentation test

A pilot solid-state fermentation plant with high reactor volumes was chosen for the test. We used reactors with a net usable volume of app. 70 l for the fermentation of soft rush silage as a single substrate (see Fig. 1b). The

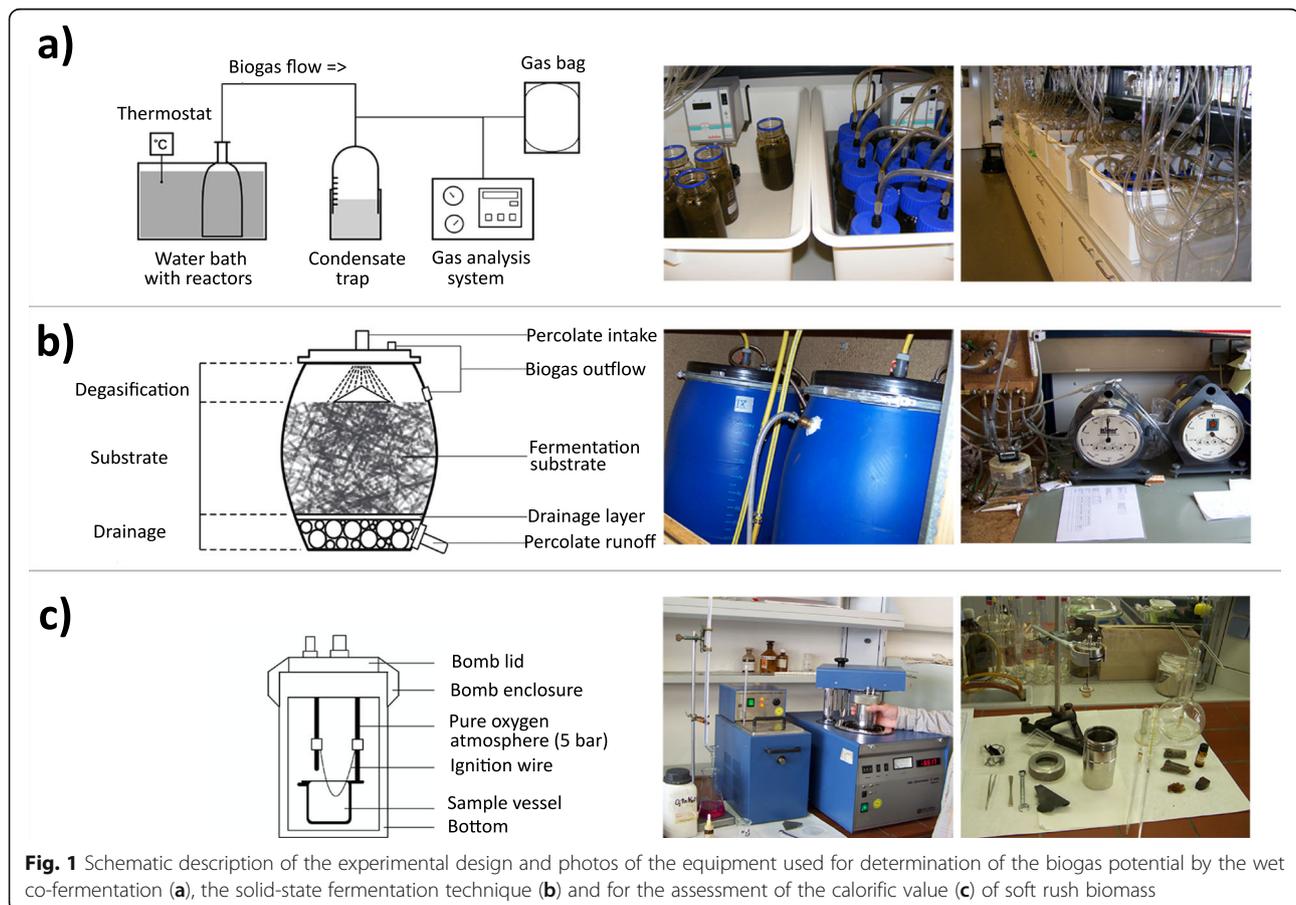


Fig. 1 Schematic description of the experimental design and photos of the equipment used for determination of the biogas potential by the wet co-fermentation (a), the solid-state fermentation technique (b) and for the assessment of the calorific value (c) of soft rush biomass

desired mesophilic reaction temperature was achieved via a thermostat-controlled heater. The percolation liquid of every reactor is stored in single heated and stirred 30 l percolate-tanks, from which the process liquid gets pumped and distributed over the substrate stock. The organic acid-enriched percolate leaves the reactor and flows back in the storage tank, whereby a small proportion flows into the sampling nozzle. The formed biogas flows through the gas hose to a measurement place. Each reactor was assigned to a gas sampling nozzle and a drum gas meter. Temperature sensors were used to measure the gas temperature prior entering the drum gas meter. An additional installed sensor recorded the prevailing ambient temperature and the air pressure enabling us to convert the measured biogas flow rates into standard litres. According to the plant operator guidelines, a two-time percolation of 15 l per day was applied after an initially substrate jamming with the entire available percolate. The residence time of the first test run was 43 days, that of the second 61 days. Both runs were repeated twice. We controlled the fermentation process by regular measurements of the pH value and the ratio of organic acids to buffer capacity (FOS/TAC ratio). Total daily dwell, the resulting biogas volume, its composition (CH₄, CO₂, O₂) and the prevailing conditions were recorded. Biogas and methane yields were calculated based on the recorded values of gas volumes and concentrations, corrected to standard conditions (norm litres at 273 K and 1013 hPa) [36].

Combustion

The fuel technical properties of purely soft rush were determined by using a bomb calorimeter (see Fig. 1c). A thermo-gravimetric analysis (TGA) was conducted, where a small amount of the sample (max. 200 mg) was filled into an inert melting pot that is surrounded by a furnace unit and connected with a highly sensitive lab balance. A computing component controlled the target temperature programme and recorded the weight loss. The temperature programme was adjusted according to the German engineering standards DIN 51718 (water content) [37], DIN 18123 (volatile matter) [38] and DIN 51719 (ash content) [39]. The proportion of solid fuel (C-fix) was calculated as the difference between the weight of the original sample and the summed proportions of volatile components, water and ashes in accordance with DIN 18123. To classify the determined parameters, the test series were complemented by analyzing well-known regenerative fuel biomass as well as added herbaceous biomass under the same conditions. To ensure similar conditions, all samples were dried under force-vented laboratory conditions and ground up to a particle size ≤ 0.5 mm afterwards.

Energy content

The energy content was analysed by the usage of an adiabatic bomb calorimeter according to DIN 18125 [40]. With this technique, a soft rush sample was completely combusted under a high-pressure oxygen atmosphere. The released thermal energy heated up a surrounding water bath. Regarding the starting and finishing temperature of the water and the specific thermal capacity of the used bomb, the gross calorific value (H_s) can be calculated.

To determine the net calorific value (H_i) of the samples with a given water content, the thermo-gravimetrically and calorimetric analyses were performed at the same time. H_s and H_i were corrected to the water free (*wf*) as to the water and ash free (*waf*) basis (Eq. 1 and 2) taking into account the water and ash content from the thermo-gravimetrically analysis. Every thermo-gravimetric and calorimetric analysis of each samples had been repeated twice consecutively.

$$H_s, H_i(wf) = \frac{H_s, H_i \times 100}{100 - w} \quad (\text{Eq.1})$$

$$H_s, H_i(waf) = \frac{H_s, H_i \times 100}{100 - w - a} \quad (\text{Eq.2})$$

Comparative parameters

We use two different approaches to compare the different conversion paths with each other. The first one, the 'Specific biogas yield potential', is limited to both bio-digestive methanation processes. The second, the 'Heat generation potential', follows a broader approach.

Specific biogas yield potential

We compared wet and solid-state fermentation techniques with the help of the specific biogas yield potential according to Weißbach [41]. We used the extent to which the nutritive-justified fermentation potential of the test substrate has been achieved as a benchmark for the conversion suitability of the process.

The potential for methane formation was estimated based on biochemical parameters of the substrates before ensiling as follows:

$$VS = 1000 - (CA) - 0.62(EULOS) - 0.000221(EULOS)^2 \quad (3)$$

$$BGY = 0.80 (VS) \quad (4)$$

$$CH_4Y = 0.42 (VS) \quad (5)$$

BGY and CH₄Y are given in norm litre per kilogramme (L_N kg DM⁻¹) and are corrected of volatile fatty acids (VFA).

Heating generation potential (HGP)

The potential of a digested substrate to generate heat as a uniform energetic measure was based on the mean calorimetric value of a normed volume of methane ($L_N CH_4$) following standard emphasis [42]:

$$HGP = 9.969 (L_N CH_4 kg^{-1}) \quad (6)$$

HGP is given in $kWh kg oDM^{-1}$.

Data analysis

Data records of interest were first tested for normal distribution using the Shapiro-Wilk test and transformed if necessary. Differences in substrate characteristics and energy yields between conversion techniques were analysed by ANOVA followed by post hoc test of the means (Tukey HSD, $p < 0.05$). Scripts using the R environment, version 3.3.2, performed all statistical analysis [43].

Results

Biochemical characteristics of the initial substrates

Due to the different test application cycles and site backgrounds, the soft rush biomass used for the individual conversion pathways was not identical. Table 2 gives an overview of the biochemical composition of the rush biomasses depending on its use. The dry matter (DM) content of the solid-state application (40.1%) is due to the preceding wilting phase as part of silage preparation. The untreated (“fresh”) biomass for the wet fermentation experiment was even higher in DM (45.5%) because of the higher physiological development stage of the rushes at the time of sampling and a further water release during transport to the lab. The rush growths for the combustion tests were technically dried to ensure good combustion suitability.

The two manually harvested biomasses (that for wet fermentation and combustion) showed no soil adhesions and had very low crude ash contents. The combined consideration of crude fibre (CF) and crude protein (CP) content served as a proxy for assessing the plant development stage. The high CF and low CP content of the

biomass intended for wet fermentation indicated an advanced degree of ripeness compared to the biomass for solid-state fermentation. The physiologically younger but ensiled biomass intended for solid-state fermentation showed even a higher content of enzyme-insoluble organic substance (EULOS) as a more lignified and thus more recalcitrant fraction in bio-digestion processes.

Wet fermentation batch tests

The cumulative development of gas formation from the tested soft rush substrate is shown in Fig. 2. The measured values are shown there in standard litres per unit of volatile solid in order to achieve the best possible comparability with other measurement results.

From about day 5 onwards, the gas formation processes in the batch vessels have stabilised. The further development of gas formation took place quasi-linearly over a period of approx. 25 days (Fig. 2a). Remarkably, a slight increase in gas formation was observed from the 30th to the termination of the experiment on the 35th incubation day. The described trend of gas formation hardly varied between the three repetitions. The dynamics of methane formation (Fig. 2b) was only slightly behind the total biogas formation in the first week, but followed the same trend thereafter.

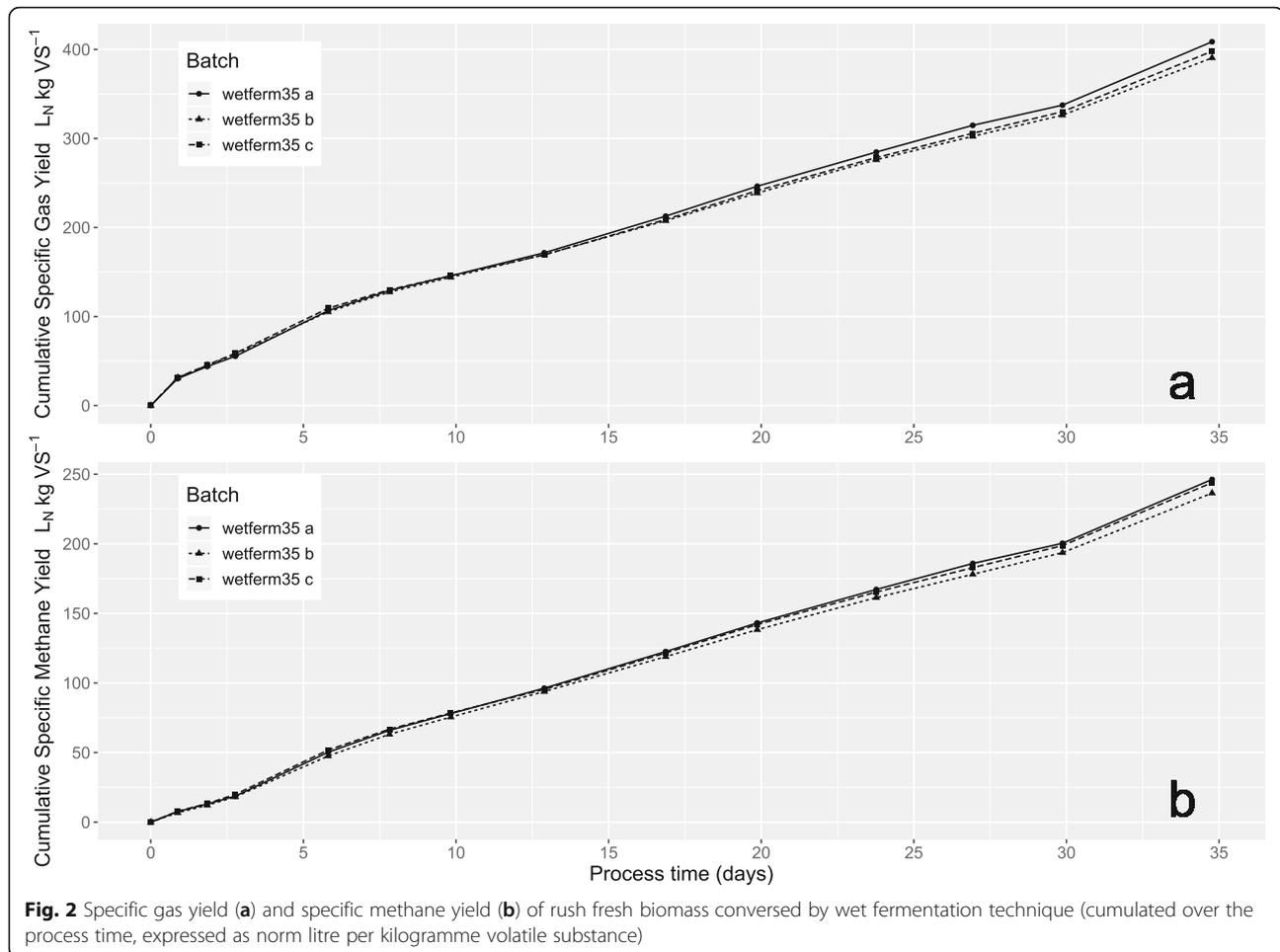
The summarised results of the standardised batch test according to the VDI Guideline 4630 are presented in Table 3. We added up the daily-determined gas production and subtracted the proportion of gas from the inoculation sludge (control) from the yield of the substrate to be examined. It should be noted that the presented values refer to the entire test duration of 35 days. This is important because such batch tests with higher-energy substrates are often run with a restricted test duration of 30 days.

After 35 days of digestion, an average of $172 L_N kg^{-1}$ FM or $399 L_N kg^{-1}$ oDM biogas was obtained from the substrate examined (Table 3). Table 3 also shows the proportion of methane in the biogas volumes formed, which is important for the quality of the gas produced and thus its later use.

Table 2 Biochemical characteristics of the conditioned rush biomass prior to their use in different energy conversion routes (means from two laboratory repetitions with standard deviations in parentheses)

Substrate condition and application purpose	Dry matter content (% FM)	Crude ash (% DM)	C (% DM)	S (% DM)	Enzyme-insoluble organic substance (EULOS $g kg^{-1}$ DM)	Crude fibre (% DM)	Crude protein (% DM)
Silage for solid-state fermentation	40.14 [2.17]	5.46 [0.18]	44.17 [0.02]	0.22 [0.003]	489.80 [63.01]	29.72 [2.74]	11.94 [1.42]
Fresh biomass for wet fermentation	45.53 [0.14]	3.03 [0.01]	45.12 [0.01]	0.18 [0.002]	456.97 [14.32]	33.43 [0.25]	7.86 [0.01]
Dried biomass for combustion	97.93 [0.08]	2.92 [0.12]	na	na	na	na	na

na not analysed



Solid-state fermentation tests

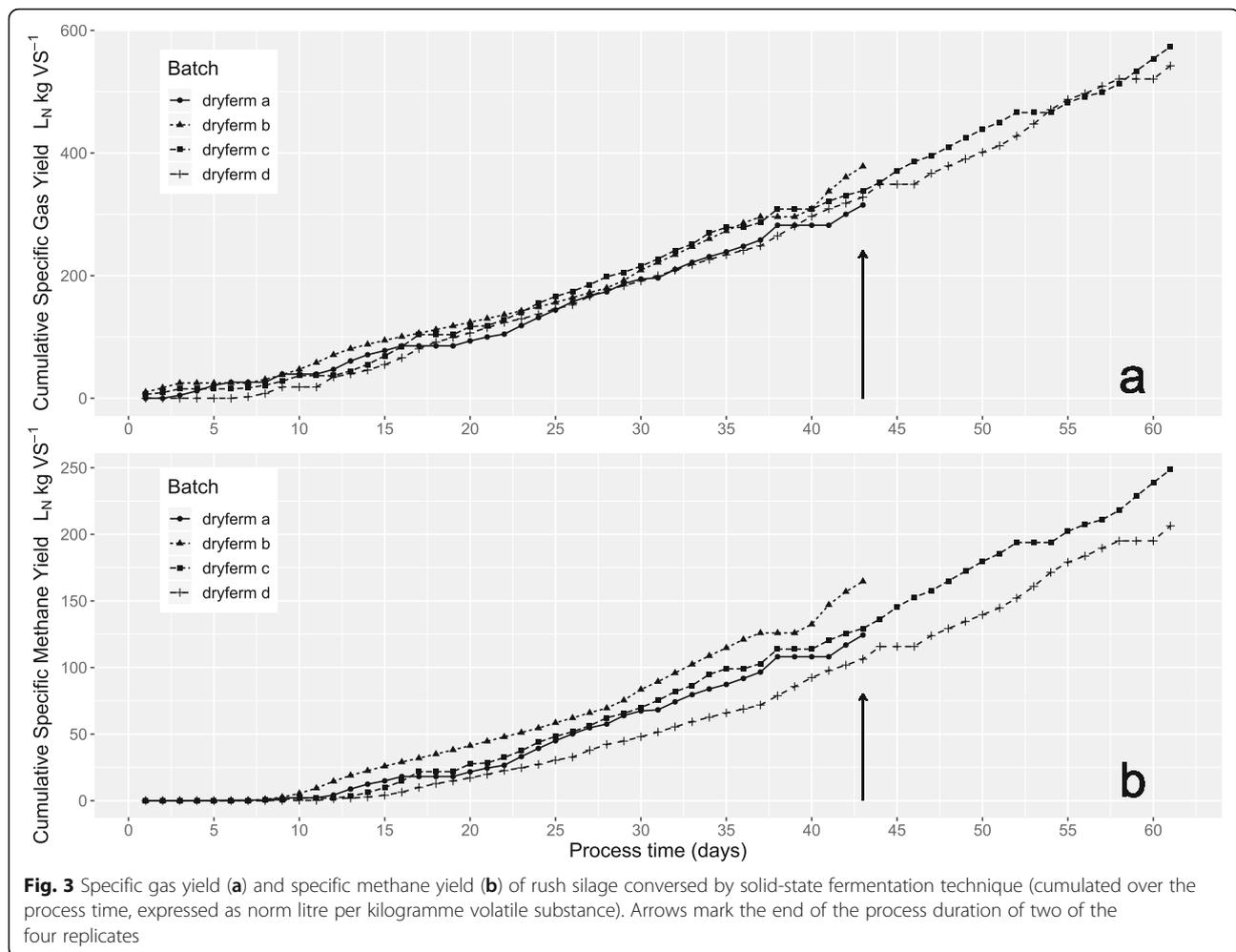
The cumulative gas formation from ensiled soft rush biomass in a solid-state fermentation set up is shown in Fig. 2. In the first two repetitions, which were stopped as planned on the 43rd day, a progressive trend of gas formation rates could be observed. Therefore, the next two repetitions were fermented over a longer period of 61 days. It is noteworthy that the gas formation curves did not flatten even at the end of the extended fermentation time.

It is apparent that the single replications differed in their fermentation yields and that these variations

increased as the experiment progressed. Methane formation (Fig. 3b) lagged behind biogas formation in the first 2 weeks after loading and then developed adequately for gasification as a whole. This led to slowly increasing methane concentrations, which only reached values above 50% after 14 days. The pH values (6.4–8.2) and FOS/TAC ratios (0.02–0.04), however, were within the normal range. Loading rates varied between replications in a range of 45.02 to 52.25 g oDM per litre. Summarised results of the solid-state fermentation tests are given in Table 4.

Table 3 Final specific biogas (BG) and methane (CH₄) yields of pure soft rush (*Juncus effusus*) after 35 days of wet co-digestion. Gas yields are given in standard norm litres (L_N) per kilogramme of fresh matter (FM) and per kilogramme of ash excluded organic dry matter (oDM)

Substrate (replication)	L _N BG kg FM ⁻¹	L _N BG kg oDM ⁻¹	L _N CH ₄ kg FM ⁻¹	L _N CH ₄ kg oDM ⁻¹	CH ₄ Vol.%
<i>Juncus effusus</i> (a)	176.65	408.64	106.44	246.23	60.3
<i>Juncus effusus</i> (b)	168.81	390.51	102.20	236.43	60.5
<i>Juncus effusus</i> (c)	172.00	397.89	105.44	243.92	61.3
Mean (sd)	172.48 (3.22)	399.02 (7.44)	104.69 (1.81)	242.19 (4.18)	60.7 (0.43)



Combustion tests

The results of the thermo-gravimetric and calorimetric analysis (TGA) are shown in Table 5. In order to allow the readers a comprehensive comparison with other biomass-based fuels and corresponding data, both gross caloric values and calorific values were presented with different reference bases.

The material used for the TGA was advertised by hand and oven-dried to get reliable gross caloric values. On

the other hand, these procedures resulted in artificial harvest conditions and a composition of the biomass that does not correspond to that produced under practical conditions. For this reason, plausible assumptions regarding crude ash content (8% DM) and residual moisture (15% DM) have been made in a further step and the net calorific value of the rush biomass based on them (H_i) has been recalculated ($15.06 \text{ MJ kg FM}_{w15}^{-1}$). We present this calculation together with compositional data

Table 4 Final specific biogas (BG) and methane (CH_4) yields of silage made from pure soft rush (*Juncus effusus*) as a single solid-state fermentation substrate. Gas yields are given in standard norm litres (L_N) per kilogramme of fresh matter (FM) and per kilogramme of ash excluded organic dry matter (oDM)

Substrate (replication)	Resident time	$L_N \text{ BG kg FM}^{-1}$	$L_N \text{ BG kg oDM}^{-1}$	$L_N \text{ CH}_4 \text{ kg FM}^{-1}$	$L_N \text{ CH}_4 \text{ kg oDM}^{-1}$
<i>Juncus effusus</i> (a)	43	119.98	315.23	47.34	124.38
<i>Juncus effusus</i> (b)	43	143.99	378.30	62.67	164.66
<i>Juncus effusus</i> (c)	61	218.17	573.19	94.60	248.55
<i>Juncus effusus</i> (d)	61	206.42	542.34	78.53	206.31
Mean (sd)	43	131.99 (12.01)	346.77 (31.54)	55.01 (7.66)	144.52 (20.14)
Mean (sd)	61	212.30 (5.88)	557.77 (15.43)	86.57 (8.04)	227.43 (21.12)

Table 5 Gross calorific values (H_s) and net calorific values (H_i) of dried soft rush (*Juncus effusus*) biomass with different reference values regarding water and ash contents. Results of the thermo-gravimetric and calorimetric analysis (TGA)

Fuel substrate	w%	DM%	CA%	H_s	$H_{s(wf)}$	$H_{s(waf)}$	H_i	$H_{i(wf)}$	$H_{i(waf)}$
<i>Juncus effusus</i> (a)	2.15	97.85	3.03	18.276	18.624	19.150	18.263	18.610	19.136
<i>Juncus effusus</i> (b)	1.96	98.04	3.01	18.276	18.667	19.199	18.263	18.654	19.185
<i>Juncus effusus</i> (c)	2.10	97.90	2.99	18.541	18.949	19.485	18.528	18.936	19.471
Mean (sd)	2.07 (0.08)	97.93 (0.08)	3.01 (0.02)	18.364 (0.12)	18.747 (0.14)	19.278 (0.15)	18.351 (0.12)	18.733 (0.14)	19.264 (0.15)

and calorific value of rush biomass compared to other common biomass-based fuels in Table 6. It should be noted that all data of the reference fuels were also obtained in the same laboratory with the same methods.

The net calorific values of the rushes even proved to be superior to those of the most common herbaceous biomasses used as fuel. This was mainly due to the high values of volatile matter (Table 6).

Comparison of conversion routes

Finally, we evaluated the tested conversion paths according to the degree of energy recovery achieved. In a first step, we compared the two processes of wet fermentation and solid-state fermentation based on the same basic principle of methanation. We used specific methane yield per weight unit of volatile solid as a measure to compare the two fermentation techniques (see Fig. 4). The most common and known high-yielding substrate, maize silage, was included in the comparison as a reference standard. The amount of the specific biogas yield potential of the maize substrate according to Weißbach [41] was exactly in the range of our wet fermentation measurements. However, this did not apply to the fermented rush biomass. The distance between the mean values (bars) and the estimates of the methane potential based on the composition of the substrates (yellow dots) can be regarded as a measure of conversion efficiency.

With a 35-day residence time in the process of wet fermentation, the methane formation potential of the soft rush could be exploited to about 90%. The solid fermentation process requires a significantly longer residence time to reach this exploitation range. After 43 days, only 58% of the expected methane potential of the pure rush silage could be harvested with the solid-state lab equipment we used.

In a second step, the combustion variant is included in the comparison of the conversion paths by converting the specific methane yield of the fermentation variants into their heating generation potential. The results of these calculations are shown in Fig. 5. The ranking of the methanisation variants is the same as that of the specific methane yields, since this is merely a conversion with a constant factor (see Equation 6 in the methods chapter) towards the heating value.

The H_i -value of 5.39 kWh kg oDM⁻¹ presented as the combustion bar in Fig. 5 is not far away from the gross calorific value and thus represents a kind of biomass-inherent energy maximum. In this sense, the diagram shows that about half of the material energy content of the rush biomass could be tapped by methanation. In other words: half of the energy was still in the digestate.

Discussion

General features of rush biomass as an energy substrate

Worthwhile areas with rush-infested or even dominated wet grassland can be found in Northern, Western and Central Europe, especially in the large fen lowlands with extensive use and nature conservation constrains, but also on blanket bogs. In many wetlands of the world, tall growing representatives of the genus *Juncus* predominate, perhaps the best known being the Everglades. From a purely quantitative point of view, the extent of retention and phytoremediation areas based on rush vegetation is still small, but is attracting increasing attention, especially in Asia.

The composition of each plant, including the soft rush, changes in the course of phenological development. From an economic point of view, however, early developmental stages are irrelevant for biomass production because they are associated with insufficient harvest

Table 6 Composition and net calorific values of biomass from rushes compared to other common biomass-based fuels

Kind of biomass	Crude ash (% DM)	Volatile matter (% oDM)	C-fix (% oDM)	$H_{i(wf)}$ (MJ kg DM ⁻¹)	H_i (MJ kg FM _{w15} ⁻¹)	H_i (kWh kg FM _{w15} ⁻¹)	
Herbaceous	Soft rush	3.01 (0.02)	80.59	19.43 (1.95)	18.73 (0.14) [17.22] ^a	15.06	4.18
	Hay	6.00 (0.26)	79.71	20.29 (0.23)	16.59 (0.19)	14.10	3.92
	Straw	8.35 (0.09)	79.44	20.56 (0.35)	16.60 (0.01)	14.11	3.92
Wood	Pine	0.24 (0.05)	82.23	17.77 (0.27)	20.07 (0.19)	15.96	4.43
	Oak	0.34 (0.13)	78.87	21.13 (0.77)	17.56 (0.23)	14.92	4.15

^aassumption: crude ash content of 8% DM as expected under harvest conditions in practice

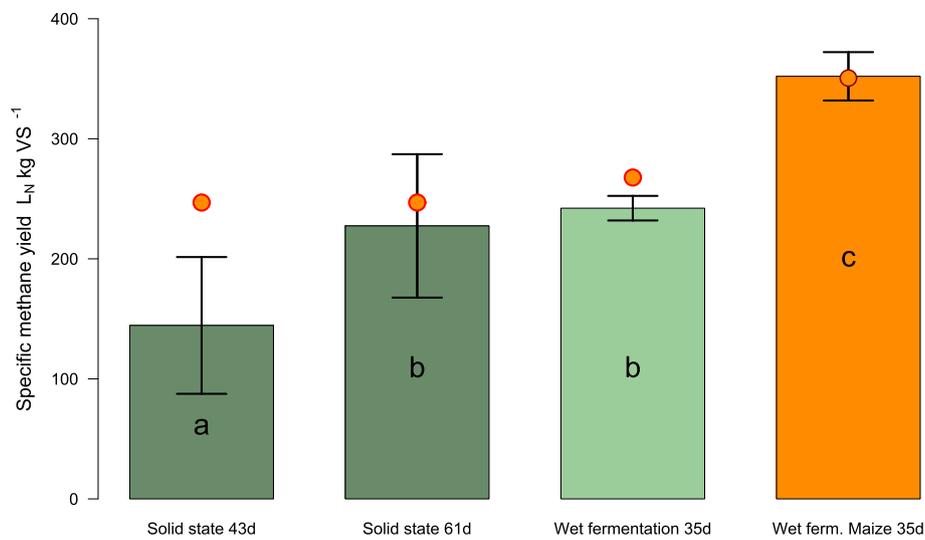


Fig. 4 Mean specific methane yield (L_N kg VS⁻¹) of different fermented soft rush biomass compared with maize as a reference co-substrate. Different letters indicate significant differences of the means (Tukey's HSD, $p < 0.05$). Error bars indicate standard deviations of the means. Dots mark the amount of specific biogas yield potential according to Weißbach [41]

yields [44]. In addition, wetlands where rush-dominated stands develop have a limited trafficability in spring when groundwater levels are high [45]. Therefore, the description of the composition of the rush biomass can be limited to developed plant stands of rushes and thus claim a certain general validity.

Our results have shown that harvest-worthy rush-dominated stands are characterised by relatively high C contents, low N contents and slightly increased S contents compared to other herbaceous plants. For the two methanation processes, the specific C-containing organic compounds are much more relevant than the C content [41, 46]. We found high cell wall proportions and

relatively few soluble carbohydrates, whereby the latter are largely used up in ensiling. Rush biomass has a high EULOS content indicating limited success of microbiological depolymerisation of these cell walls during digestion. According to Weißbach [47], enzyme-insoluble organic substance correlates negatively with the methane yield. Although the lignin content was not explicitly determined in this study, the constellation of high cell wall contents and limited enzymatic solubility indicates a high degree of lignification of the older plant parts. While this content pattern does not promise optimal conditions for methanisation, it suggests a high calorific value when used as a solid biofuel.

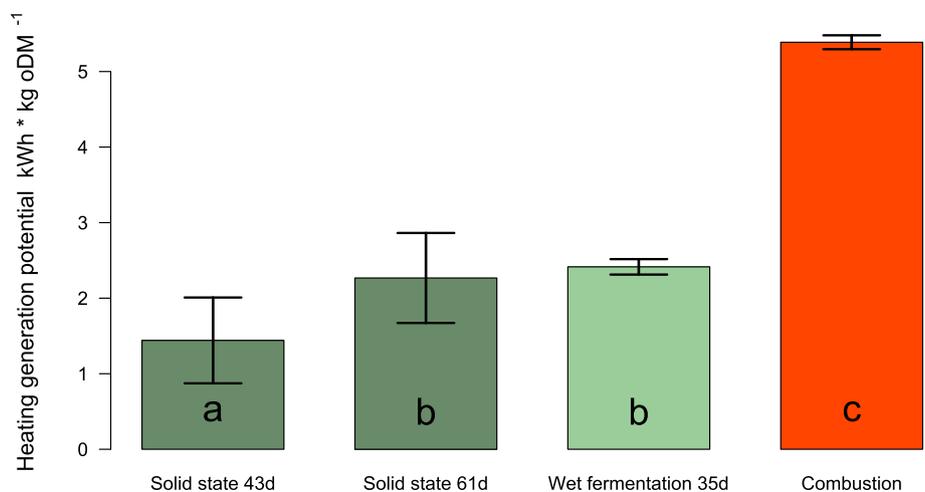


Fig. 5 Comparison of the heating generation potential (kWh kg DM⁻¹) of soft rush biomass in different conversion routes. Different letters indicate significant differences of the means (Tukey's HSD, $p < 0.05$). Error bars indicate standard deviations of the means

For a successful application of rush biomass in incineration plants, however, not only the calorimetric energy content but also the dry matter content and the mineral composition plays a pivot role. One difficulty in the field drying of rushes for combustion purpose is the wet conditions of their preferred habitats. Dry periods at late summer must therefore be consistently exploited for rush hay preparation. Where the target dry matter content of 80% cannot be achieved by field drying, precautions must be taken for subsequent drying under rain shelter conditions. According to Joseph et al. [34], mineral composition of wet grassland vegetation dominated by rushes does not differ significantly from that of other extensive grassland growths. However, this may be not true in the case of origins from coastal [48] or retentional [17, 49] areas. For example, *Juncus gerardii* as a halophytic salt marsh rush contains significantly higher contents of Na and Cl than *Juncus effusus* in inland areas [50]. When recovering rushes from phytoremediation applications [16], it must be assumed that the phosphorus content of the rush biomass exceeds that of natural populations [13, 18] and that heavy metals and organic complexing agents are also present [17], whose behaviour in the individual conversion techniques is largely unknown. Further research is needed on this issue.

Another special feature of rush biomass is its physical structure. Rush tillers are characterised by aerenchyma which allow gas diffusion through the tissues [51]. This property could, even in chopped condition, have an influence on certain utilisation processes such as the oxygen supply during combustion or the methane removal during anaerobic fermentation. These hitherto unexplored aspects would be worth a closer look.

While the majority of semi-natural grassland areas infested with rushes also contain certain proportions of grasses and herbs and thus represent mixed biomass stands, in the case of retention areas and conceivable paludicultures, these are pure stands. For the latter, the results of this study can be used directly. In the case of mixed biomasses, further investigations with targeted variation of the accompanying flora are necessary in order to be able to reliably estimate the energetic exploitation potential.

Evaluation of rush biomass as substrate in special conversion routes

Wet fermentation

For our knowledge, we presented first results of specific biogas yield of biomass from rushes as substrate in wet fermentation process here. With a specific methane yield of 242 L_N kg⁻¹ oDM, a level was achieved which corresponds to that of other substrates from landscape management growths [52, 53]. Nearly 90% of the expected

methane potential of the soft rush biomass could be tapped in 35 days retention time. Since the methane formation curve did not flatten out even towards the end of the experiment, we assume that the wet fermentation process is able to almost completely tap the methane formation potential. However, the residence time in continuous-flow plants, which dominate in practice, will probably not be sufficient to achieve the maximum energy yield. In addition, the wet fermentation plants must be designed in such a way that floating of the aerenchyma-containing material in the premix pit is prevented. A short chop length, which is highly recommended for rush biomass, also contributes to avoid this loading problem. It cannot be assumed that the operating concept of a wet fermentation biogas plant is based on rush biomass as the main substrate. Nevertheless, the use of rush biomass as a component of a co-substrate mixture seems practicable.

Solid-state fermentation

Solid-state fermentation techniques are not widely used in farm practice, but occur in waste management. An advantage of these plants for lignocellulose-rich biomasses is the longer residence time [54] and the associated possibility of accelerating microbial catabolic processes [55]. Therefore, hopes for an economic exploitation of landscape management biomasses rest on this conversion technique. In our study, these hopes could not be fulfilled by using ensiled rush biomass as the sole substrate. The obvious reason was the delayed formation of methane in the initial phase of fermentation, a problem that other experimenters using solid-state techniques also reported [56, 57]. As reasons for the restrained methane formation after loading, hyperacidity (VFA overload) [54] and too high ammonium concentrations [58] are listed. We can exclude both causes for our experiments. It is likely that our test facility will require an optimisation of the sprinkler technology in the start-up phase as well as an inoculum that originated from cultures of the test substrate. Despite these limitations, we still see potential for increasing conversion efficiency in the solid-state fermentation process. For example, the percolation frequency can be increased. Also, the use of rush biomass as a pure substrate does not appear to be very useful. In previous investigations on the same experimental set-up, the advantages of rush biomass as a mixing partner for grassland crops could be demonstrated [59]. Therefore, in contrast to the results of the wet fermentation experiment, we consider our measurement results for the solid-state conversion of the rush biomass to be rather lower guide values, which could be exceeded in practice.

Combustion

In the absence of further data on the calorific value of rushes, comparison with other biomass-based fuels helps to classify the results. We found that the net calorific value of dried biomass from soft rush exceeds that of the most common herbaceous solid fuels, straw and hay. This finding is mainly due to the relatively high content of volatile matter in the rush biomass, while the fixed carbon content was similar to that of the herbaceous reference fuels. A high proportion of volatile matter in turn makes the rush biomass also interesting for pyrolysis processes, which we have not considered here. When evaluating the heating values of rush biomass, it must be taken into account that the raw ash contents are unusually low due to manual harvesting. But even assuming a more realistic raw ash content of 8% and a residual moisture content of 15% of the fuel, the net calorific value of $15.06 \text{ MJ kg FM}_{w15}^{-1}$ is still attractive for thermal conversion. While the calorific value shows a potential, its implementation in terms of incineration technology remains a challenge. Profound knowledge of the chemical composition and physical properties of the ashes is necessary for optimising combustion process [60]. The composition of the ash in turn depends on the mineral pattern [61], which was not fully investigated in the study presented.

Benefits and prospects of using rush biomass for bioenergy production

Biochemical properties and realised energy yields of biomasses from rush dominated wetland stands do not show rushes as excellent energy plants, which is why there are no efforts to cultivate them for energetic purposes actually. However, this is not even necessary, as rush biomass is produced anyway in the course of landscape and nature conservation management. If we take the nutrient retention areas additionally into account, which also require the removal of biomass for nutrient export purposes, we obtain a promising energy reservoir free of opportunity costs. Seen in this light, the use of such kind of biomass integrated into an overall social concept can be regarded as an example of modern land use policy [62]. From a societal point of view, the main advantage of the production of bioenergy from rush-dominated wetland biomass is its potential to combine renewable energy policies and landscape conservation goals while avoiding competition with food and forage production.

Nevertheless, the exploitation of these potentials is not easy, especially because of the scattered location of the rush infested wetland sites in a given landscape context. It cannot be assumed that the operating concept of a bioenergy plant is based on rush biomass as main substrate. What we have been able to show with our results is that it is possible to use various conversion routes with rush biomass as a substrate. For this purpose, the advantages and

disadvantages of the specific material properties of the rush biomass for the respective conversion path must be known and considered accordingly in the process design. This study has made a contribution to this.

Conclusions

In this paper, we analysed the use of biomass from soft rush (*Juncus effusus* L.) in three different conversion routes. We used largely standardised and thus comparable methods for the conversion paths of wet fermentation and combustion as well as a less common technique for determining substrate suitability in the solid-state fermentation technique. According to our results and from a pure calorimetric point of view, the energy potential of rush growths at a developed physiological stage can best be exploited by combustion, whereas biodigestive approaches are at a disadvantage from the outset due to the high proportion of poorly degradable cell wall structures. Nevertheless, fermentation techniques have also been able to achieve energy yields that are not below those of other waste biomasses from landscape management. In addition, the high proportion of recalcitrant C compounds in the fermentation residues can also be an advantage in supplying agricultural soils with a stable C source. This kind of C fixation may also be beneficial to prevent CO₂ losses and thus could act as a further contribution of a climate-friendly sustainable energy policy besides reducing greenhouse gas emissions generated from competing fossil fuels. Low costs for substrate production make energetic utilisation of rush stands an interesting alternative, if short distances between fields and biomass conversion plant can be realised. In Germany, the probability of short transport distances between wetlands with rush dominated stands and existing energy conversion techniques is much greater for biogas plants than for incineration plants. In order to increase the transportability of rushes as solid fuel, the biomass would have to be pelleted or briquetted, which causes additional costs. The preferability of such processed solid biofuels depends on the cost development in the field of fossil fuel carriers.

Solid-state fermentation is particularly suitable if the use of biomass from landscape management in a larger wetland complex is to be integrated into an ecological land use concept including extensive animal farming with farmyard manure as a further solid substrate. This technology still has development potential, but must be built cost-effectively in order to be economically viable. The current suppliers of technically mature plants do not meet this economical requirement. Finally, besides the size of the rush dominated area, and the distribution of these areas in the landscape, the investment costs and the subsidies for the conversion plant play a pivotal role in the selection of the preferred conversion process.

Abbreviations

BG: Biogas; BGY: Biogas yield; C: Carbon; CA: Crude ash; CF: Crude fibre; C-fix: Proportion of solid fuel; CH₄: Methane; CH₄Y: Methane yield; CP: Crude protein; DM: Dry matter; EULOS: Enzyme-insoluble organic substance; FM: Fresh matter; FOS: Volatile organic acids; HGP: Heat generation potential; H_c: Gross calorific value; H_v: Caloric value; kWh: Kilowatt hour; L_N: Standard norm litre; oDM: Ash excluded organic dry matter; S: Sulphur; TAC: Total alkaline carbonates (buffer capacity); TGA: Thermo-gravimetric analysis; VFA: Volatile fatty acids; VS: Volatile solids (fermentable organic matter); w%: Water content; wf: Water free; waf: Water and ash free

Acknowledgements

We dedicate this contribution to the initiator of this special issues 'Sustainable use of aquatic macrophytes for the production of bioenergy', Prof. Andreas Zehnsdorf, who encouraged us to make this contribution and unfortunately died far too early. We are grateful to Kristof Habermann who participated in the wet fermentation part of our investigation. Moreover, we thank the reviewers of this journal, who provided us with critical and thorough feedback to improve the quality of this contribution.

Authors' contributions

JM and CJ contributed to the conception and the design of the study. DW organised and administrated the wet fermentation experiments and did the efficiency calculations. CJ was responsible for the solid-state and combustion measurements. JM wrote the first draft of the manuscript. CJ and DW supplemented and improved the manuscript. JM performed the statistical analysis in coordination with CJ and DW. All authors contributed to manuscript revision and read and approved the submitted version.

Funding

One measurement run of solid fermentation was taken from material generated in the project 'Restoration of species-rich moor grassland through a sustainable agricultural use with special regard on the soft rush problem', funded by the German Federal Foundation for the Environment DBU (Deutsche Bundesstiftung Umwelt, grant number: 23063/01). All other data sets were obtained within the framework of student graduation theses without external financial support.

Availability of data and materials

All relevant data is contained within the manuscript. In addition, raw data from processed data will be made available by the authors, without undue reservation, to any qualified researcher on request.

Ethics approval and consent to participate

Not applicable.

Consent for publication

All participants consented the confidential publication of their contributions in this study.

Competing interests

The authors declare that they have no competing interests.

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Received: 2 January 2020 Accepted: 24 June 2020

Published online: 23 July 2020

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